

# Modeling & Numerical Simulation of Hypersonic Flows

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**ERCOFTAC Autumn Festival 2023**

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# Developing disruptive technology for hypersonics

- ▶ Hypersonics
  - ▶ Fight within planetary atmosphere at Mach  $> 5$
- ▶ Challenges for fluid models and numerical methods
  - ▶ Multiscale and multiphysics problem
  - ▶ Calibration and validation of computational models



Air Breathing Electric Propulsion concept  
for Very Low Earth Orbit observation



Orion Crew Module reentry  
14 November 2022 (Artemis I)

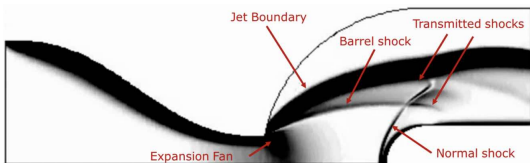
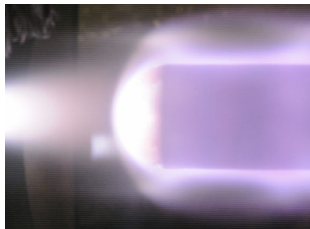
# “Aerothermochemistry” coined by von Kármán

*“With the advent of jet propulsion, it became necessary to broaden the field of aerodynamics to include problems which before were treated mostly by physical chemists. . .”*

Theodore von Kármán, 1958

## ► Some open problems

- Fluid models for thermo-chemical nonequilibrium
- High-order methods for hypersonic flows
- Efficient solvers for 3D plasma sheath



[Capriati, Turchi, Congedo, M., 9th EUCASS 2022]

Under-expanded air jet over catalytic probe in VKI Plasmatron



# MUlticomponent Thermodynamic And Transport properties for IONized gases library written in C++

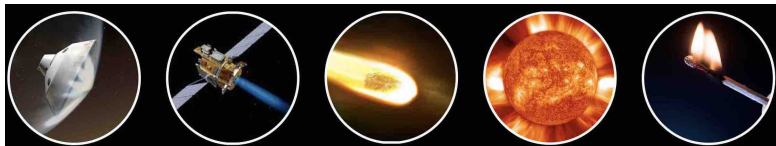
## M<sup>++</sup> Mutation

Multicomponent Thermodynamic And Transport properties for IONized gases in C++

<https://github.com/mutationpp/Mutationpp>

[Scoggins, Leroy, Bellas-Chatzigeorgis, Dias, M., Software X 2017]

- ▶ Centralizes physico-chemical models, algorithms, and data for reactive and plasma flows into a single software package
- ▶ Can be shared among CFD tools



# Outline

Coarse-grain transport models consistent from the kinetic to fluid regimes

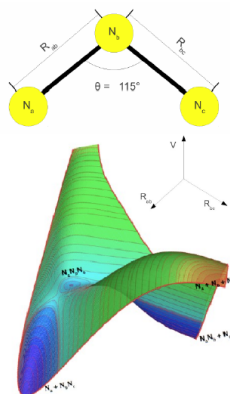
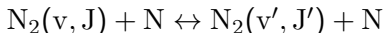
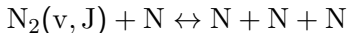
Simulation of plasma sheath

Atmospheric entry simulation

Calibration of models

# Microscopic approach to derive macroscopic nonequilibrium models...

- ▶ Developing high-fidelity models physics-based
- ▶ NASA ARC database for nitrogen chemistry
  - ▶ 9390  $(v, J)$  rovibrational energy levels for  $N_2$
  - ▶  $50 \times 10^6$  reaction mechanism for  $N_2 + N$  system



$N_3$  Potential Energy Surface

NASA Ames Research Center

# Kinetic equation for coarse-grain model

[Torres, Bellas-Chatzigeorgis, M., Physics of Fluids, 2021]

- ▶ Set of species

$$\mathcal{S} = \{N, N_2(k) \mid (k = 1, 2, \dots, n_{\text{bins}})\}$$

- ▶ Boltzmann equation (1D space 3D velocity)

$$\frac{\partial f_N}{\partial t} + c_x \frac{\partial f_N}{\partial x} = \frac{1}{\varepsilon} \mathcal{J}(f_N, f_N) + \frac{1}{\varepsilon} \sum_{l \in \mathcal{K}_{N_2}} \mathcal{J}(f_N, f_l) + \varepsilon \mathcal{C}_N$$

$$\frac{\partial f_k}{\partial t} + c_x \frac{\partial f_k}{\partial x} = \frac{1}{\varepsilon} \mathcal{J}(f_k, f_N) + \frac{1}{\varepsilon} \sum_{l \in \mathcal{K}_{N_2}} \mathcal{J}(f_k, f_l) + \varepsilon \mathcal{C}_k, \quad k \in \mathcal{K}_{N_2}$$

- ▶ Reactive collisions are assumed to follow the Maxwellian regime
- ▶ Consistency between the kinetic and fluid regimes is a direct consequence of the asymptotic analysis of the Boltzmann eq.



# Fluid regime: Navier-Stokes eqs.

- ▶ Enskog expansion

$$f_i = f_i^0(1 + \varepsilon\phi_i), \quad i \in \mathcal{S}$$

- ▶ Chapman-Enskog perturbative solution method yields

$$\frac{\partial \rho_N}{\partial t} + \frac{\partial}{\partial x} (\rho_N u + \rho_N u_N^d) = \omega_N$$

$$\frac{\partial \bar{\rho}_k}{\partial t} + \frac{\partial}{\partial x} (\bar{\rho}_k u + \bar{\rho}_k \bar{u}_k^d) = \bar{\omega}_k, \quad k \in \mathcal{K}_{N_2}$$

$$\frac{\partial \rho u}{\partial t} + \frac{\partial}{\partial x} (\rho u^2 + p - \tau_{xx}) = 0$$

$$\frac{\partial \rho E}{\partial t} + \frac{\partial}{\partial x} \left( \rho u \left( E + \frac{p}{\rho} \right) - \tau_{xx} u + q_x \right) = 0$$

- ▶ Chemical production rates satisfy the law of mass action
- ▶ The forward and backward rate coefficients are linked to an equilibrium constant consistent with the system thermodynamics

## Entropy eq. (2nd law of thermodynamics)

$$\frac{\partial(\rho s)}{\partial t} + \frac{\partial}{\partial x}(\rho s u) + \frac{\partial}{\partial x} J_S = \Upsilon$$

### ► Entropy flux

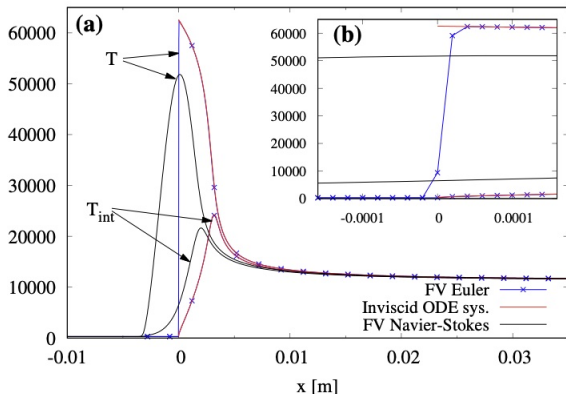
$$J_S = \frac{q}{T} - \sum_{k \in \mathcal{K}_{N_2}} \bar{\rho}_k \bar{u}_k^d \frac{\bar{g}_k}{T} - \rho_N u_N^d \frac{g_N}{T}$$

### ► Entropy production

$$\Upsilon \geq 0$$

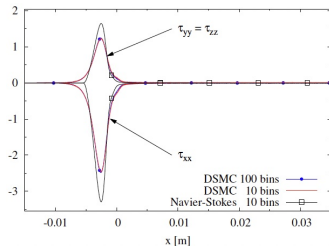
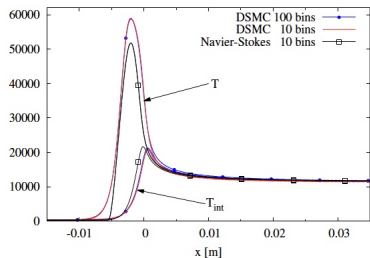
- First coarse-grain model equipped with a transport theory that satisfies the laws of thermodynamics

# Viscous (Navier-Stokes) versus inviscid (Euler) solution (shock wave, $u = 10$ km/s)



- ▶ Euler FV solutions not polluted by numerical diffusion
- ▶ Any diffusive effects observed in the Navier–Stokes profiles are physical in nature, i.e., exclusively due to the actual molecular diffusion terms

# Viscous (Navier-Stokes) versus DSMC solution (shock wave, $u = 10$ km/s)



- ▶ For these flight conditions, good agreement found between kinetic (DSMC) and fluid (CFD) solutions
- ▶ Consistency of the cross-sections / rate coefficients is crucial

# Outline

Coarse-grain transport models consistent from the kinetic to fluid regimes

Simulation of plasma sheath

Atmospheric entry simulation

Calibration of models

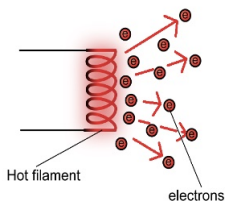
# Plasma-wall interaction: sheath

## ► Sheath

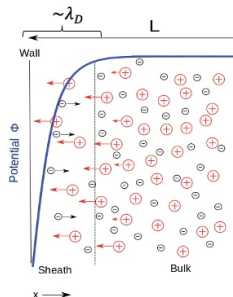
- Layer in a plasma which has a greater density of positive ions

## ► Challenges

- Sheath thickness becomes small as pressure increases
- Multifluid models become expensive as number of species increases



Thermionic emission used in electron transpiration cooling



# Dimensional analysis for plasmas [Petit, Darrozes 1975]

- ▶ 2 kinetic temporal scales based on common mean-free-path  $l^0$

$$t_e^0 = \frac{l^0}{V_e^0}, \quad t_h^0 = \frac{l^0}{V_h^0} = \frac{1}{\epsilon} t_e^0 \quad \text{with} \quad \epsilon = \frac{V_h^0}{V_e^0} = \sqrt{\frac{m_e}{m_h}}$$

- ▶ 1 macroscopic temporal scale based on macroscopic length  $L^0$

$$t^0 = \frac{L^0}{V_h^0} = \frac{1}{Kn} t_h^0 \quad \text{with} \quad Kn = \frac{l^0}{L^0}$$

## Nondimensional form and scaling of Boltzmann eq.

- ▶ Electrons:  $e$

$$\partial_t f_e + \frac{1}{\varepsilon} \mathbf{c}_e \cdot \partial_{\mathbf{x}} f_e + \frac{1}{\varepsilon} q_e \mathbf{E} \cdot \partial_{\mathbf{c}_e} f_e = \frac{1}{\varepsilon Kn} [\mathcal{J}_{ee}(f_e, f_e) + \sum_{j \in H} \mathcal{J}_{ej}(f_e, f_j)]$$

- ▶ Heavy particles:  $i \in H$

$$\partial_t f_i + \mathbf{c}_i \cdot \partial_{\mathbf{x}} f_i + \frac{q_i}{m_i} \mathbf{E} \cdot \partial_{\mathbf{c}_i} f_i = \frac{1}{Kn} \left[ \frac{1}{\varepsilon} \mathcal{J}_{ie}(f_i, f_e) + \sum_{j \in H} \mathcal{J}_{ij}(f_i, f_j) \right]$$

- ▶ Multiscale asymptotic analysis with entangled parabolic and hyperbolic scalings [Graille, M., Massot 2009]

$$\varepsilon = Kn$$

- ▶ **Electrons:** low Mach number regime

[Bardos, Golse, Levermore, 1991]

- ▶ **Heavy particles:** compressible gas dynamics regime

[Goudon, Jabin, Vasseur, 2005]



# Multifluid scaling of Boltzmann eq.

- ▶ Kinetic equation for species  $i \in S$

$$\partial_t f_i + \mathbf{c}_i \cdot \partial_{\mathbf{x}} f_i + \frac{\mathbf{F}_i}{m_i} \cdot \partial_{\mathbf{c}_i} f_i = \sum_{j \neq i} \mathcal{J}_{ij}(f_i, f_j) + \frac{1}{\epsilon} \mathcal{J}_{ii}(f_i, f_i) + C_i^r$$

- ▶ Fluid equations are decoupled for each species
- ▶ Example: isothermal ion - electron mixture in neutral bath

$$\begin{aligned}\partial_t n_e + \partial_x (n_e u_e) &= n_e \nu^{iz} \\ \partial_t n_i + \partial_x (n_i u_i) &= n_e \nu^{iz} \\ \partial_t (n_e u_e) + \partial_x \left( n_e u_e^2 + \frac{p_e}{m_e} \right) &= \frac{n_e e}{m_e} \partial_x \phi - n_e u_e \nu_{en} \\ \partial_t (n_i u_i) + \partial_x \left( n_i u_i^2 + \frac{p_i}{m_i} \right) &= -\frac{n_i e}{m_i} \partial_x \phi - n_i u_i \nu_{in}\end{aligned}$$

- ▶ Coupling to Poisson's eq.

$$\partial_{xx}^2 \phi = \frac{e(n_e - n_i)}{\epsilon_0}$$

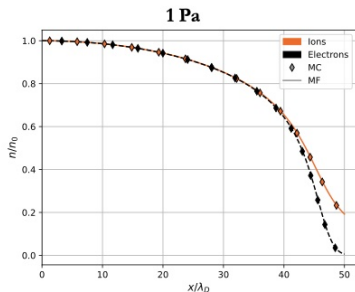
# Comparison multifluid / multicomponent diffusion models

## ▶ Binary diffusion model

$$\partial_t n_e + \partial_x (n_e V_e) = n_e \nu^{iz}$$

$$\partial_t n_i + \partial_x (n_i V_i) = n_e \nu^{iz}$$

- ▶ Diffusion velocity:  $V_k = -\frac{D_k}{n_k} \partial_x n_k - \mu_k \partial_x \phi$
- ▶ Binary diffusion coefficient:  $D_k = \frac{k_B T_k}{m_k \nu_{kn}}$
- ▶ Species mobility:  $\mu_k = \frac{q_k}{m_k \nu_{kn}}$

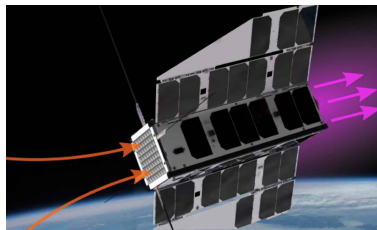


Simulation of 1D plasma sheath at 1 Pa between 2 walls

[Gangemi, Alvarez Laguna, Hillewaert, M., 9th EUCASS 2022]

# Air-Breathing Electric Propulsion (ABEP)

- ▶ Residual atmosphere drag compensated by thrust
- ▶ ABEP systems collect atmospheric molecules through intake
- ▶ Air propellant for electric thruster, no lifetime limitation!

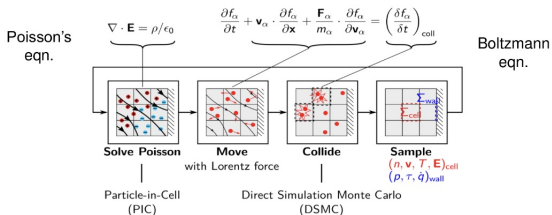
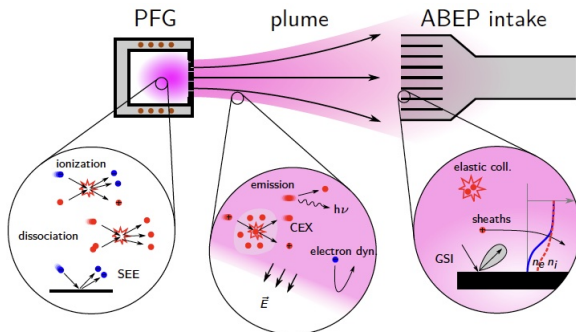


Air Breathing Electric Propulsion concept  
for Very Low Earth Orbit observation



VKI DRAGON low-density facility

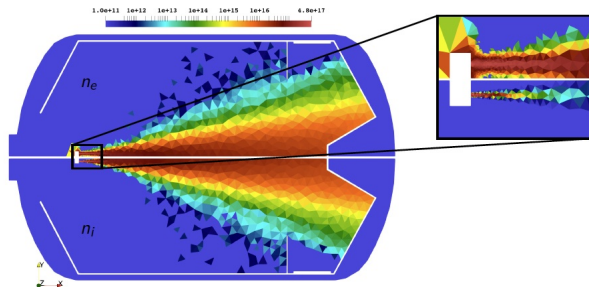
# PIC/DSMC plasma simulation (PANTERA code)



[Parodi, Lapenta, M., GEC 2022]

# Plasma plume simulation with semi-implicit scheme

- ▶ Plasmas of our interest span multiple length- and time scales
- ▶ With an explicit PIC scheme no choice but to resolve these
- ▶ Fully-implicit methodology with Jacobian computed from the actual particle motion in the grid



[Parodi, Lapenta, M., GEC 2022]

# Outline

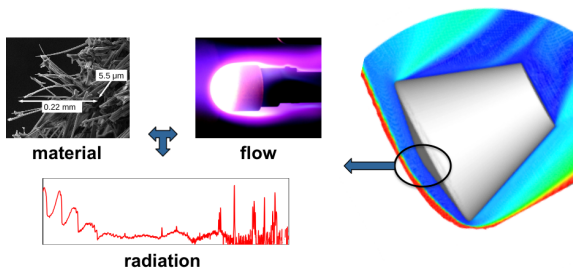
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**Atmospheric entry simulation**

Calibration of models

# Development of integrated codes for flow / radiation / material coupling



- ▶ Ablative material / flow coupling  
Pyrolysis gas blows in the boundary layer
- ▶ Flow / radiation coupling  
Radiation field depends on flow excited species concentration
- ▶ Ablative material / radiation coupling  
Ablation products can absorb the shock layer radiation

# Apollo 4 peak heating trajectory point

- ▶ First flight of Saturn V rocket and all-up test of Apollo systems (unmanned)
- ▶ Ablative TPS
- ▶ Radiometer aligned at stagnation point
- ▶ Fore body was a 33 $\frac{1}{2}$  sphere segment with nose radius of 4.69 m
- ▶ Equivalent sphere radius of 2.85 m to reproduce shock standoff distance [Park, 2004]



Time s	Altitude km	$V_\infty$ km/s	$\rho_\infty$ kg/m <sup>3</sup>	$T_\infty$ K
30020	67.47	10.640	$1.13 \cdot 10^{-4}$	224.53
30024	64.55	10.511	$1.73 \cdot 10^{-4}$	232.71
30028	61.99	10.382	$2.50 \cdot 10^{-4}$	239.88
<b>30032</b>	<b>59.79</b>	<b>10.252</b>	<b><math>3.41 \cdot 10^{-4}</math></b>	<b>246.04</b>
30036	58.00	10.042	$4.31 \cdot 10^{-4}$	251.05
30040	56.69	9.798	$5.01 \cdot 10^{-4}$	254.72
30044	55.89	9.534	$5.51 \cdot 10^{-4}$	256.96

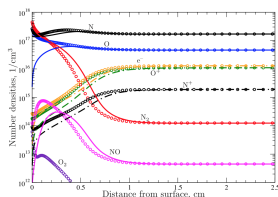
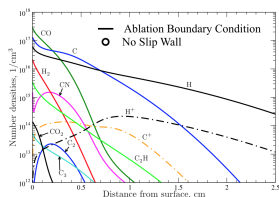


# Simulation of Apollo 4 peak heating trajectory point

Coupling strategy	$\epsilon(\sigma T^4 + q_w^{\text{rad}})$ W/cm <sup>2</sup>	$\epsilon q_w^{\text{rad}}$ W/cm <sup>2</sup>	$q_w^{\text{diff}}$ W/cm <sup>2</sup>	$q_w^{\text{cond}}$ W/cm <sup>2</sup>	$q_w^{\text{conv}}$ W/cm <sup>2</sup>	$\dot{m}(h_w - h_s)$ W/cm <sup>2</sup>
Flow	-91.64	-279.92	-2.70	-119.77	-122.47	-
Flow / Abl.	-66.46	-254.74	-38.62	-95.31	-133.93	5.99
Flow / Rad.	-8.36	-196.64	-4.56	-168.42	-172.98	-
Fully Coupled	-6.16	-194.44	-37.77	-97.38	-135.15	5.79

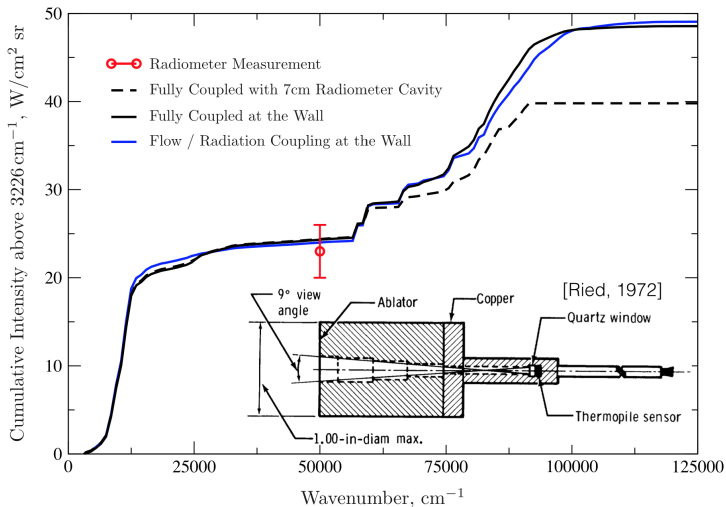
[Scoggins, PhD thesis 2017]

- ▶ Shock layer radiative cooling due to strong plasma emission
- ▶ Ablation products released by the heat shield contribute to increased radiation blockage in the boundary layer



⇒ Strong coupling between the flow / radiation / material fields

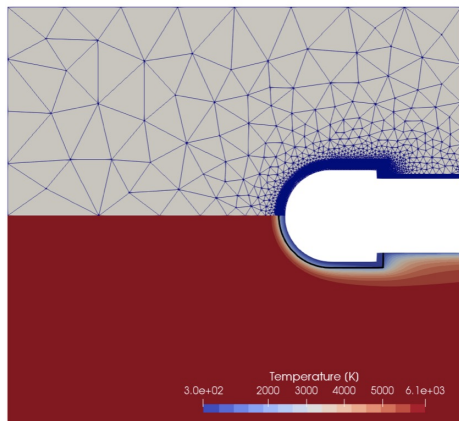
# Comparison to radiometer flight data



# Development of a unified solver to treat reactive porous material and high enthalpy flows

## ► Implementation in the Argo code (CENAERO)

[Schrooyen, Dias, Fagnani, Turchi, Helber, Walpot, M., FAR 2022]



Mass :

### ▪ Gas

$$\frac{\partial \epsilon_g \langle \rho_i \rangle_g}{\partial t} + \nabla \cdot (\epsilon_g \langle \rho_i \rangle_g \langle u \rangle_g) = \nabla \cdot \left( \epsilon_g \frac{D_{i,m}}{\eta} \langle \rho_i \rangle_g \frac{W_i}{W} \nabla X_i \right) + \langle \dot{\omega} \rangle + \Pi_g$$

### ▪ Solid (fibers + char + resin)

$$\frac{\partial \epsilon_s \langle \rho_s \rangle_s}{\partial t} = \langle \dot{\omega}^{het} \rangle - \Pi_g$$

Momentum :

$$\frac{\partial (\epsilon_g \langle \rho u \rangle_g)}{\partial t} + \nabla \cdot (\epsilon_g \langle \rho \rangle_g \langle u \rangle_g \langle u \rangle_g) = -\epsilon_g \nabla \langle P \rangle_g + \nabla \cdot \langle \tau \rangle + F$$

Energy :

$$\frac{\partial \langle \rho E_{tot} \rangle}{\partial t} + \nabla \cdot (\epsilon_g \langle \rho \rangle_g \langle H \rangle_g \langle u \rangle_g) = \nabla \cdot (\lambda_{eff} \nabla T) + \nabla \cdot \langle (\tau \cdot u) \rangle$$

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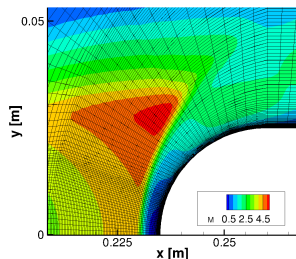
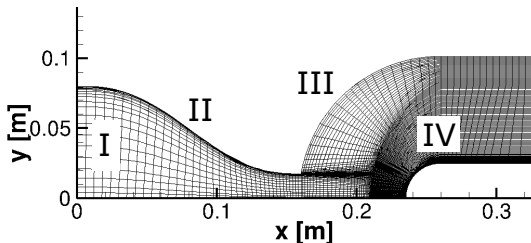
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# US3D CFD solver for hypersonic flows (U Minnesota)

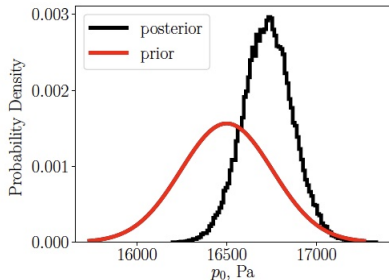
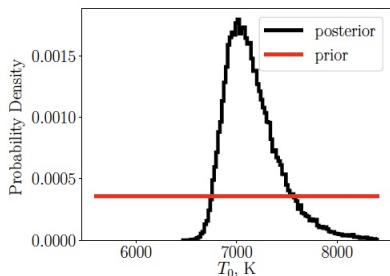
- ▶ 3D Finite-Volume discretization
- ▶ Modified Steger-Warming numerical scheme with MUSCL reconstruction
- ▶ Data Parallel Line Relaxation (DPLR) to obtain rapid convergence to steady-state



**Left:** computational domain I) exit of plasma torch, II) sonic nozzle surface, III) expansion chamber and IV) probe. **Right:** zoom on numerical grid adapted with the shock to avoid carbuncle

# Multifidelity surrogate model based on hierarchical Kriging

Tag	cells	$\Delta x$ [m]	$h_i$	$t_{CPU}$ [min]
I	172224	5E-7	1	$\approx 1600$
II	43056	1E-6	2	$\approx 200$
III	10764	2E-6	4	$\approx 30$
IV	2691	4E-6	8	$\approx 4$

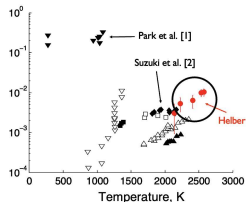


Prior and posterior marginal distributions for the Qols.

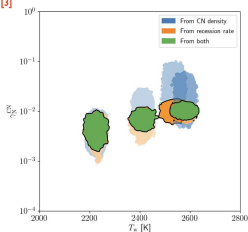
[Capriati, Turchi, Congedo, M., 9th EUCASS 2022]

# Stochastic calibration of carbon nitridation model from plasma wind tunnel experiments

Nitridation Probability

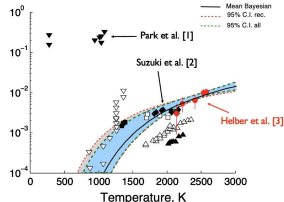


Bayesian inference  
methodology



[del Val, Lemaitre, Congedo, M., Carbon 2022]

Nitridation Probability



Integration of all available  
measurements from Helber *et al.*

$$\gamma_N^{\text{CN}} = A \exp\left(\frac{-T_a}{T_w}\right)$$

# Conclusion

- ▶ Hypersonics is a multiscale and multiphysics problem
- ▶ Kinetic theory is a powerful tool to derive sound fluid models for plasmas
- ▶ Well identified mathematical structure of the conservation eqs. allows for development of numerical schemes
- ▶ Don't forget to calibrate and validate your computational models!



# Thank you!

- ▶ Collaborators who contributed to the results presented
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  - ▶ Giovanni Lapenta (KULeuven)
  - ▶ Nagi Mansour (NASA Ames)
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